# Methodology and Experience in Applying a Non-Destructive Testing Method by Barkhausen Noise Analysis, for Example, in Ion-Treated Samples

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*Abstract.* The present paper expresses the idea of the possibility of using a non-destructive method of research by means of Barkhausen Noise Analysis (BNA – Barkhausen Noise Analysis), replacing the conventional destructive methods for the examination of nitrided layers, making evaluations and comparisons with them. The paper refers to a specially created methodology, the implementation of which consistently follows the presentation of the paper. Comparing the non-destructive testing methodology with tribological, mechanical and metallographic research can outline which of the analyses can be substituted and what accuracy can be relied upon for the substitution. Heat-resistant steel BH21 was used as the object of research.

The research is of practical value because the process has been established for this steel. The experience gained in this regard will help to expand and validate non-destructive testing methods.

Keywords: Ion nitriding, property identification, comparison between non-destructive and destructive testing methods.

### I. INTRODUCTION

There is a wide range of fundamental and scientificapplied research in the field of methods and means of specialized methods for non-destructive testing, through which labour-intensive and time-consuming methods of destructive approaches can be replaced.

In the process of ion nitriding, because of the difference in the dimensions of the crystal structure of the different phase composition in the ion-treated layer, internal stresses arise. It has been shown that they can be characterized by analysing the characteristics of the magnetic noise [1, 2], caused by the dislocations in the microstructure in the examined ferromagnetic material. The information provided by these characteristics enables differentiated

processing of the information used to evaluate the multiparameter analysis of the nitriding mode and other types of processing of each individual input parameter [3, 4, 5]. This is possible thanks to the property of ferromagnetic bodies discovered by Barkhausen, whose magnetization under the action of an external magnetic field is accompanied by numerous jumps in magnetization. These jump-like changes are called Barkhausen jumps. These jumps are shown to be due to the jump-like displacement of the blast furnace walls. The domain wall is the transition boundary in a transition layer between two domains in which the magnetization spin direction gradually changes its orientation from a direction parallel to the magnetization vector of the first domain to a direction parallel to the magnetization vector of the second domain [6]. In the present research, the assessment is made by comparing traditional characteristics with those of magnetic noise caused by the Barkhausen effect, which according to expert opinion [7] is considered promising.

Apart from that, the authors have their own developed computational approach [8], which has proven its efficiency in the research of problems from engineering technologies. In addition to individual optimization calculations, it can also be used for identification of examined quality indicators, including for non-destructive technologies.

The brief review of the indicated research can determine the characteristic of the chosen topic, which is associated with the complexity and non-linearity of the various properties of the materials in the depth of processing of the considered surfaces. These new surface conditions are formed by a desired set of properties, which is determined by solving multicriteria problems [8, 9]. The latter guarantee certain benefits of the research, most often

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expressed in increased longevity (extended life) of contact products [10, 11]. All this relates to the production resource, characterization and applications in the field of hard coatings and wear-resistant surfaces.

#### II. MATERIALS AND METHODS

The present research aims to provide an idea and a methodology for applying a methodology proven in ion technology that works in practice, to be transferred to other related technologies. The chemical composition of the two steels is listed in Table 1.

TABLE 1. CHEMICAL COMPOSITION OF BH21 STEEL

Steels	С	Cr	Mo	V	W	Si	Mn	Ni	Cu	S
BH21	0,30	2,70	I	0,29	8,01	0,18	0,26			0,015

		NORMALIZED
Nitriding at temperature [°C]		Microhardness [%]
Ammonia pressure [Pa]	Research of the influence of the control parameters of the	Relative wear resistance [%]
Time of nitriding [h]	ion nitriding process on non- destructive, mechanical and	Thickness of nitrided zone and nitrided white zone [%]
Temperature of tempering [°C]	conventional destructive methods for steel BH 21	Magnetic noise value [%]

Fig.1. Input-output parameters in the statement of the problem

The influence of the technological parameters on the surface properties of BH21 steel depending on the conditions of ionic nitriding is examined. The complexity of the problem regarding identification in the technological process cited in Fig. 1 lies in the fact that there are more than two technological parameters, and the examined criteria have a different relationship to them. After establishing the relationship between technological parameters and examined criteria through the definition of the models, it is possible to apply a process of identification of surface properties depending on the processing mode. They can be evaluated by a non-destructive method. This process is established in [10, 11] by the limits of variation indicated in Table 2, by the derived models of the controlled quantities in Table 3 and by their extreme values indicated in Table 3.

TABLE 2. INTERVALS OF CHANGE OF TECHNOLOGICAL PARAMETERS

	Parameter of the	Extreme low	Average	Extreme upper		
№	technological mode of ion nitriding and	Interval value of mode change				
	preliminary heat treatment	Code [-1]	Code [0]	Code [+1]		
1	Nitriding at temperature $t_{nit} [^{\circ}C] - (X_l)$	510	530	550		
2	Ammonia pressure P <sub>NH3</sub> [Pa] – (X <sub>2</sub> )	150	300	450		
3	Time of nitriding $t [h] - (X_3)$	4	7	10		
4	Temperature of tempering $t_{tem} [^{o}C] - (X_{4})$	600	650	700		

The derivation of the models in [10, 11] was done with the methodology presented in [8], and the optimization of the models was performed with [9]. Using [9] there were produced the models shown in Table 3.

TABLE 3. COEFFICIENTS OF THE MODELS FOR THE INFLUENCE OF NITRIDING PARAMETERS ON THE VALUE OF THE INVESTIGATED CRITERIA

Coefficients	BH 21, microhardness	BH21, linked zone	BH21, wear resistance	BH21, total thickness of the nitrided zone
$b_0$	1102.94	3.66667	0.511111	257.60
$b_1 * X_1$	-7.93750	2.12500	-0.085625	33.810
$b_2 * X_2$	-3.56250	1.12500	-0.018125	-0.330
$b_3 * X_3$	3.06250	_	-0.068125	42.640
$b_4 * X_4$	-55.6875	0.8750	0.030625	-7.910
$b_5 * X_1^2$	_	-	-	0.250
$b_6 * X_1 X_2$	-3.93750	0.8750	0.0118750	0.6250
$b_7 * X_1 X_3$	3.68750	0.250	0.00437500	-6.880
$b_8 * X_1 X_4$	25.4375	-0.3750	0.010625	-0.630
$b_9 * X_2^2$	_	_	_	-19.750
$b_{10} * X_2 X_3$	-22.4375	-0.250	-0.060625	-1.870
$b_{11} * X_2 X_4$	11.0625	-0.1250	0.0081250	-5.630
$b_{12}^*X_3^2$	_	_	—	-19.750
$b_{13} * X_3 X_4$	-12.3125	-0.250	-0.0443750	-5.630
$b_{15} * X_{42}$	_	_	_	-24.750

Through the derived models when applying [10], the extremes of the steel can be determined for each of the parameters. This determined the modes in Table 4.

TABLE 4. EXTREME VALUES OF THE EXAMINED PARAMETERS

Ob- ject	Microhardness	Wear resistance	Linked zone thickness	Nitrided zone total thickness	
BH21	$ \begin{array}{r} \text{Min:} \\ 1005.82 \\ \hline X_2 = 450 \\ \hline X_3 = 10 \\ \hline X_4 = 700 \\ \end{array} $	$\begin{array}{c} X_1 = 550 \\ Min: & X_2 = 450 \\ 0.28 & X_3 = 10 \\ \hline X_4 = 600 \end{array}$	$\begin{array}{c} \text{Min:} \\ 0.33 \end{array} \begin{array}{c} X_1 = 510 \\ X_2 = 150 \\ \hline X_3 = 4 \\ \hline X_4 = 600 \end{array}$	$\begin{array}{c} X_1 = 510 \\ Min: \\ 89.235 \\ \hline X_2 = 450 \\ \hline X_3 = 4 \\ \hline X_4 = 700 \\ \end{array}$	
BH21	$\begin{array}{c} \text{Max:} & \frac{X_1 = 510}{X_2 = 150} \\ 1236.82 & \frac{X_3 = 10}{X_4 = 600} \end{array}$	$\begin{array}{c} X_1 = 510 \\ Max: X_2 = 450 \\ 0.77 \\ X_3 = 4 \\ X_4 = 600 \end{array}$	Max: $X_1 = 550$ $X_2 = 450$ $X_3 = 4$ $X_4 = 700$	$\begin{array}{c} X_1 = 550 \\ Max: & X_2 = 170 \\ 341.18 & X_3 = 10 \\ \hline X_4 = 650 \end{array}$	

This review would be more targeted if a methodology could be analytically or numerically defined to fix the influence of different modes on surfaces that are determined as destructive and non-destructive.

#### III. RESULTS AND DISCUSSION

Through non-destructive and traditional destructive testing methods, the quality of the products is ensured. Non-destructive testing methods have one significant advantage over all other control methods, which consists in checking each specific product without disturbing its integrity. For this reason, the methodology – object of this research – was created and verified.

The specific research tests the methodology by comparing the value of the measured noise with the results of the models indicated in Table 3 and the extreme values of the examined quantities indicated in Table 4. The algorithm of the methodology is shown in Fig.2.

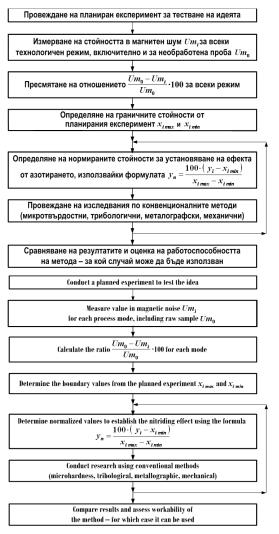


Fig.2. Methodology algorithm

The most essential part of the presented methodology is the calculation of all the examined quantities and their normalization so that the comparison itself can be realized. This is how the credibility of the results is achieved and they can be justified for the purpose of their future use.

 TABLE 5. RESULTS OF THE COMPARISON OF THE NON-DESTRUCTIVE

 CHARACTERISTIC WITH THE DESTRUCTIVE ONES

Mode No.	Umn [%]	Wear resis- tance [%]	Micro- hardnes s [%]	Thick- ness nitrided layer [%]	Thick- ness white zone [%]
$t_{\rm nit}$ =510 [°C], $P_{\rm NH3}$ = 150 [Pa], $\tau$ = 4 [h], $t_{\rm tem}$ = 700[°C]	0	15,306	35,93	9,57	31,99
t <sub>nit</sub> =530 [°C], $P_{NH3} =$ 300 [Pa], T= 2.76 [h], $t_{tem} = 650$ [°C]	32,76	36,93	40,216	37,31	41,26
$t_{\text{nit}} = 530 \ [^{\circ}\text{C}], P_{\text{NH3}} = 300 \ [\text{Pa}],$ $T = 7 \ \text{h}, \tau = 7 \ [\text{h}], t_{\text{tem}} = 650 [^{\circ}\text{C}]$	52,84	52,86	42,42	66,86	41,26
$t_{\rm nit} = 530 \ [^{\rm o}{\rm C}], \ P_{\rm NH3} = 88 \ [{\rm Pa}], \\ \tau = 7 \ [{\rm h}], \\ t_{\rm tem} = 650 \ [^{\rm o}{\rm C}]$	61,809	47,55	44,58	51,35	21,59
Absolute deviation from the normalized voltage of the measured noise		8.44	17.76	9.65	23.07

To experimentally verify the presented methodology, a real experiment was performed in which the results were compared between the characteristics of the nondestructive testing by means of Barkhausen noise analysis and those of the conventional methods of analysis. Because of the inspection, the following results were obtained.

A graphical interpretation of the results of this comparison is presented in Fig.3.

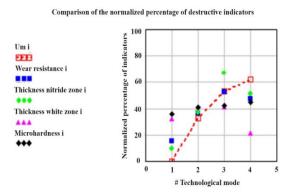


Fig.3. Graphical representation of the comparison results

From this check, the influence of the various parameters of the nitriding mode on the Barkhausen noise characteristic for steel BH21 was determined. Based on this theoretical-experimental research, the following main conclusions can be drawn, which derive directly from Table 5 and Fig. 3.

1. The maximal recoil temperature is associated with the minimally normalized Barkhausen noise characteristic for steel BH21.

2. For BH21 steel, the nitriding process time has less effect on the Barkhausen noise value for BH21 steel than the gas pressure.

3. For each of the examined quality indicators, the absolute deviation from the normalized Barkhausen noise characteristic was determined, and this result ranked the mechanical and destructive methods of analysis. The analysis of this research proves that the non-destructive Barkhausen noise settling method can be successfully applied to the relative wear resistance and the total thickness of the nitride zone for which the deviation is less than 10%.

4. For the final proof of the workability of the methodology, it is necessary to confirm these statements with nitriding under the same conditions on another steel, although the different alloy composition may lead to certain smaller or larger deviations.

#### IV. CONCLUSION

In conclusion, it is necessary to note that through the research done, the possibility of using the non-destructive research method through Barkhausen Noise Analysis (BNA) replacing the conventional destructive methods for researching nitrided layers, making evaluations and comparisons has been clarified between them. The comparison of the proposed non-destructive methodology with tribological, mechanical and metallographic research reported which of the analyzes can be replaced and what accuracy can be relied on in this replacement. The research refers to heat-resistant steel BH21. The microstructure of the nitrided layer plays an indirect role through the depth distribution of the phases. Through the study, the

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relationship between phase composition, technological mode and percentage of normalized destructive tests was found. A non-destructive test has been developed and tested, which can be an alternative to existing destructive methods. We believe that the research also has practical value because the process has been established for this steel. Such experience will help to expand and validate non-destructive control methods.

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